

### Applications

- Telecommunications
- Data communications
- Wireless communications
- Servers, workstations

### Benefits

- High efficiency – no heat sink required
- Higher current capability at elevated temperatures than competitors' 50 A quarter-bricks
- Industry-standard 1/8<sup>th</sup> brick footprint: 0.896" x 2.30" (2.06 in<sup>2</sup>) - 38% smaller than conventional quarter-bricks

### Description

The new high performance 50A SQE48T50012 DC-DC converter provides a high efficiency single output, in a 1/8<sup>th</sup> brick package that is only 62% the size of the industry-standard quarter-brick. Specifically designed for operation in systems that have limited airflow and increased ambient temperatures, the SQE48T50012 converter utilize the same pinout and functionality of the industry-standard quarter-bricks.

The SQE48T50012 converter provides thermal performance in high temperature environments that exceeds most 50A quarter-bricks in the market. This performance is accomplished through the use of patented/patent-pending circuits, packaging, and processing techniques to achieve ultra-high efficiency, excellent thermal management, and a low-body profile.

Low-body profile and the preclusion of heat sinks minimize impedance to system airflow, thus enhancing cooling for both upstream and downstream devices. The use of 100% automation for assembly, coupled with advanced electronic circuits and thermal design, results in a product with extremely high reliability.

Operating from a 36-75V input, the SQE48T50012 converter provides a 1.2V output voltage that can be trimmed from -20% to +10% of the nominal output voltage, thus providing outstanding design flexibility.

With standard pinout and trim equations, the SQE48T50012 converter is a perfect drop-in replacement for existing 50A quarter-brick designs. Inclusion of this converter in a new design can result in significant board space and cost savings. The designer can expect reliability improvement over other available converters because of the SQE48T50012's optimized thermal efficiency.

### Features

- RoHS lead-free solder and lead-solder-exempted products are available
- Delivers up to 50 A
- Industry-standard quarter-brick pinout
- On-board input differential LC-filter
- Start-up into pre-biased load
- No minimum load required
- Weight: 0.88 oz [25.1 g]
- Meets Basic Insulation requirements of EN60950
- Withstands 100 V input transient for 100 ms
- Fixed-frequency operation
- Fully protected
- Remote output sense
- Positive or negative logic ON/OFF option
- Low height of 0.374" (9.5mm)
- Output voltage trim range: +10%/-20% with industry-standard trim equations
- High reliability: MTBF =17.5 million hours, calculated per Telcordia SR-332, Method I Case 1
- UL60950 recognized in US and Canada and DEMKO certified per IEC/EN60950
- Designed to meet Class B conducted emissions per FCC and EN55022 when used with external filter
- All materials meet UL94, V-0 flammability rating

## Electrical Specifications

Conditions:  $T_A = 25\text{ }^\circ\text{C}$ , Airflow = 300 LFM (1.5 m/s),  $V_{in} = 48\text{ VDC}$ ,  $C_{in} = 33\text{ }\mu\text{F}$ , unless otherwise specified.

Parameter	Notes	Min	Typ	Max	Units
<b>Absolute Maximum Ratings</b>					
Input Voltage	Continuous	-0.3		80	VDC
Operating Ambient Temperature		-40		85	$^\circ\text{C}$
Operating Altitude	$I_{out} = 50\text{A}$			3000	m
	$I_{out} \leq 40\text{A}$	3001		10000	m
Storage Temperature		-55		125	$^\circ\text{C}$
<b>Isolation Characteristics</b>					
Standard Product: Option <b>0</b> (refer to Converter Part Numbering/Ordering Information)					
I/O Isolation		2250			VDC
Isolation Capacitance			160		pF
Isolation Resistance		10			$\text{M}\Omega$
Option <b>K</b> (refer to Converter Part Numbering/Ordering Information)					
I/O Isolation		1500			VDC
Isolation Capacitance			1200	1500	pF
Isolation Resistance		10			$\text{M}\Omega$
<b>Feature Characteristics</b>					
Switching Frequency			330		kHz
Output Voltage Trim Range <sup>1</sup>	Industry-std. equations	-20		+10	%
Remote Sense Compensation <sup>1</sup>	Percent of $V_{OUT(NOM)}$			+10	%
Output Overvoltage Protection	Non-latching	117	132	147	%
Overtemperature Shutdown (PCB)	Non-latching		125		$^\circ\text{C}$
Operating Humidity	Non-condensing			95	%
Storage Humidity	Non-condensing			95	%
Peak Back-drive Output Current (Sinking current from external source during startup into pre-biased output)	Peak amplitude			50	mADC
Back-drive Output Current (Sinking Current from external source)	Converter OFF; external voltage 5 VDC		10	50	mADC
Auto-Restart Period	Applies to all protection features		200		ms
Turn-On Time	See Figs. E, F, and G		3	6	ms
ON/OFF Control (Positive Logic)					
Converter Off (logic low)		-20		0.8	VDC
Converter On (logic high)		2.4		20	VDC
ON/OFF Control (Negative Logic)					
Converter Off (logic high)		2.4		20	VDC
Converter On (logic low)		-20		0.8	VDC

Additional Notes:

<sup>1</sup>  $V_{out}$  can be increased up to 10% via the sense leads or 10% via the trim function. However, the total output voltage trim from all sources should not exceed 10% of  $V_{OUT(NOM)}$ , in order to ensure specified operation of overvoltage protection circuitry.

**Electrical Specifications (continued)**

Conditions:  $T_A = 25\text{ }^\circ\text{C}$ , Airflow = 300 LFM (1.5 m/s),  $V_{in} = 48\text{ VDC}$ ,  $C_{in} = 33\text{ }\mu\text{F}$ , unless otherwise specified.

Parameter	Notes	Min	Typ	Max	Units
<b>Input Characteristics</b>					
Operating Input Voltage Range		36	48	75	VDC
Input Undervoltage Lockout					
Turn-on Threshold		33.5		35.5	VDC
Turn-off Threshold		31.5		33.5	VDC
Lockout Hysteresis Voltage			2.0		VDC
Input Voltage Transient	100 ms			100	VDC
Input Voltage Transient Rate				7	V/ms
Inrush Transient Rating				0.1	A <sup>2</sup> s
Maximum Input Current	50 ADC Out @ 36 VDC In $V_{OUT} = 1.2\text{ VDC}$			2.1	ADC
Input Stand-by Current	$V_{in} = 48\text{V}$ , converter disabled		2.5		mA
Input No Load Current (0A load on the output)	$V_{in} = 48\text{V}$ , converter enabled $V_{OUT} = 1.2\text{ VDC}$		25		mA
Input Reflected-Ripple Current, $i_s$	$V_{in} = 48\text{V}$ , 25 MHz bandwidth $V_{OUT} = 1.2\text{ VDC}$		12		mA <sub>PK-PK</sub>
Input Voltage Ripple Rejection	120 Hz, $V_{OUT} = 1.2\text{ VDC}$		60		dB

**Electrical Specifications (continued)**

Conditions:  $T_A = 25\text{ }^\circ\text{C}$ , Airflow = 300 LFM (1.5 m/s),  $V_{in} = 48\text{ VDC}$ ,  $C_{in} = 33\text{ }\mu\text{F}$ , unless otherwise specified.

Parameter	Notes	Min	Typ	Max	Units
<b>Output Characteristics</b>					
External Load Capacitance	Plus full load (resistive)			20,000	$\mu\text{F}$
Output Current Range		0		50	ADC
Current Limit Inception	Non-latching	52		65	ADC
Peak Short-Circuit Current	Non-latching, Short = 10 m $\Omega$		55		A
RMS Short-Circuit Current	Non-latching		17		Arms
Output Voltage Set Point (no load) <sup>2</sup>		-1		+1	%Vout
<b>Output Regulation</b>					
Over Line			$\pm 2$	$\pm 5$	mV
Over Load			$\pm 2$	$\pm 5$	mV
Output Voltage Range	Over line, load and temperature <sup>2</sup>	-3.0		+3.0	%Vout
Output Ripple and Noise – 25 MHz bandwidth	Full load + 10 $\mu\text{F}$ tantalum + 1 $\mu\text{F}$ ceramic $V_{OUT} = 1.2\text{ VDC}$		40	60	mV <sub>PK-PK</sub>
<b>Dynamic Response</b>					
Load Change 50%-75%-50% of Iout Max, di/dt = 0.1 A/ $\mu\text{s}$	$C_o = 1\text{ }\mu\text{F}$ ceramic (Figure 8)		20		mV
di/dt = 2.5 A/ $\mu\text{s}$	$C_o = 470\text{ }\mu\text{F}$ POS + 1 $\mu\text{F}$ ceramic		70		mV
Settling Time to 1% of Vout			15		$\mu\text{s}$
<b>Efficiency</b>					
100% Load	$V_{OUT} = 1.2\text{ VDC}$		83		%
50% Load	$V_{OUT} = 1.2\text{ VDC}$		89		%
<b>Mechanical</b>					
Weight			25.1g		
Vibration IEC Class 3M5	Freq. Velocity IEC 68-2-6	5-9Hz 5mm/s			
	Freq. Accelerat. IEC 68-2-6	9-200Hz 1g			
Shocks IEC Class 3M5	Accelerat. IEC 68-2-29	10g			
	MIL-STD-202F	Method 213B Cond. F			
<b>Reliability</b>					
MTBF	Telcordia SR-332, Method I Case 1 50% electrical stress, 40 $^\circ\text{C}$ components	17.5			MHrs
	Telcordia SR-332, Method I Case 1 $V_{IN} = 48\text{V}$ , $I_{OUT} = 25\text{A}$ , 400LFM, $T_{AMB} = 25\text{ }^\circ\text{C}$	14.58			MHrs

Additional Notes:

<sup>2</sup> Operating ambient temperature range of -40  $^\circ\text{C}$  to 85  $^\circ\text{C}$  for converter..

## Operations

### Input and Output Impedance

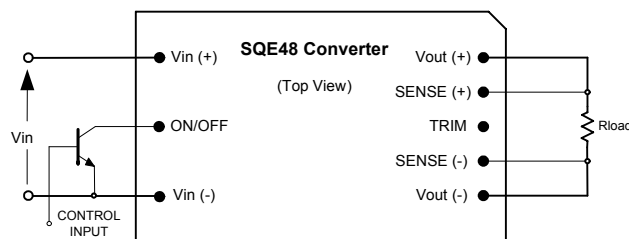
These power converters have been designed to be stable with no external capacitors when used in low inductance input and output circuits.

However, in some applications, the inductance associated with the distribution from the power source to the input of the converter can affect the stability of the converter. A 33  $\mu\text{F}$  electrolytic capacitor with an ESR  $< 1 \Omega$  across the input is recommended to ensure stability of the converter.

In many applications, the user has to use decoupling capacitance at the load. The power converter will exhibit stable operation with external load capacitance up to 20,000  $\mu\text{F}$ .

### ON/OFF (Pin 2)

The ON/OFF pin is used to turn the power converter on or off remotely via a system signal. There are two remote control options available, positive and negative logic, with both referenced to  $V_{in(-)}$ . A typical connection is shown in Fig. A.



**Fig. A: Circuit configuration for ON/OFF function.**

The positive logic version turns on when the ON/OFF pin is at a logic high and turns off when at a logic low. The converter is on when the ON/OFF pin is left open. See the Electrical Specifications for logic high/low definitions.

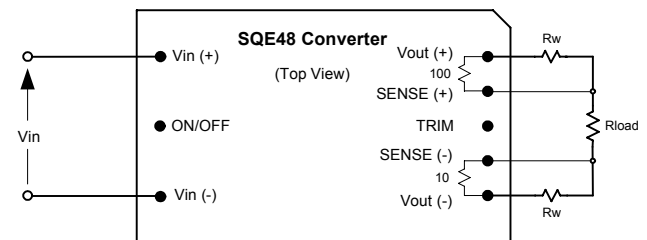
The negative logic version turns on when the pin is at a logic low and turns off when the pin is at a logic high. The ON/OFF pin can be hard wired directly to  $V_{in(-)}$  to enable automatic power up of the converter without the need of an external control signal.

The ON/OFF pin is internally pulled up to 5 V through a resistor. A properly de-bounced mechanical switch, open-collector transistor, or FET can be used to drive the input of the ON/OFF pin. The device must be capable of sinking up to 0.2 mA at a low level voltage of  $\leq 0.8 \text{ V}$ . An external voltage source ( $\pm 20 \text{ V}$  maximum) may be connected directly to the ON/OFF input, in which case it must be capable of sourcing or sinking up to 1 mA depending

on the signal polarity. See the Startup Information section for system timing waveforms associated with use of the ON/OFF pin.

### Remote Sense (Pins 5 and 7)

The remote sense feature of the converter compensates for voltage drops occurring between the output pins of the converter and the load. The SENSE(-) (Pin 5) and SENSE(+) (Pin 7) pins should be connected at the load or at the point where regulation is required (see Fig. B).



**Fig. B: Remote sense circuit configuration.**

### CAUTION

If remote sensing is not utilized, the SENSE(-) pin must be connected to the  $V_{out(-)}$  pin (Pin 4), and the SENSE(+) pin must be connected to the  $V_{out(+)}$  pin (Pin 8) to ensure the converter will regulate at the specified output voltage. If these connections are not made, the converter will deliver an output voltage that is higher than the specified data sheet value.

Because the sense leads carry minimal current, large traces on the end-user board are not required. However, sense traces should be run side by side and located close to a ground plane to minimize system noise and ensure optimum performance.

The converter's output overvoltage protection (OVP) senses the voltage across  $V_{out(+)}$  and  $V_{out(-)}$ , and not across the sense lines, so the resistance (and resulting voltage drop) between the output pins of the converter and the load should be minimized to prevent unwanted triggering of the OVP.

When utilizing the remote sense feature, care must be taken not to exceed the maximum allowable output power capability of the converter, which is equal to the product of the nominal output voltage and the allowable output current for the given conditions.

When using remote sense, the output voltage at the converter can be increased by as much as 10% above the nominal rating in order to maintain the required voltage across the load. Therefore, the designer must, if necessary, decrease the maximum current (originally obtained from the derating curves) by the same percentage to ensure the converter's

actual output power remains at or below the maximum allowable output power.

**Output Voltage Adjust /TRIM (Pin 6)**

The output voltage can be adjusted up 10% or down 20%, relative to the rated output voltage by the addition of an externally connected resistor.

The TRIM pin should be left open if trimming is not being used. To minimize noise pickup, a 0.1 μF capacitor is connected internally between the TRIM and SENSE(-) pins.

To increase the output voltage, refer to Fig. C. A trim resistor, R<sub>T-INCR</sub>, should be connected between the TRIM (Pin 6) and SENSE(+) (Pin 7), with a value of:

$$R_{T-INCR} = \frac{5.11 \times (100 + \Delta) \times V_{O-NOM}}{0.6\Delta} - \frac{511}{\Delta} - 10.22 \text{ [k}\Omega\text{]},$$

where,

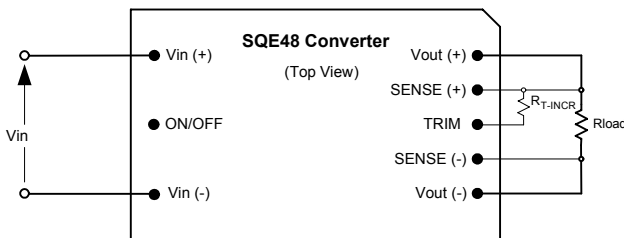
R<sub>T-INCR</sub> = Required value of trim-up resistor kΩ

V<sub>O-NOM</sub> = Nominal value of output voltage [V]

$$\Delta = \left| \frac{(V_{O-REQ} - V_{O-NOM})}{V_{O-NOM}} \right| \times 100 \quad [\%]$$

V<sub>O-REQ</sub> = Desired (trimmed) output voltage [V].

When trimming up, care must be taken not to exceed the converter's maximum allowable output power. See the previous section for a complete discussion of this requirement.



**Fig. C: Configuration for increasing output voltage.**

To decrease the output voltage (Fig. D), a trim resistor, R<sub>T-DECR</sub>, should be connected between the TRIM (Pin 6) and SENSE(-) (Pin 5), with a value of:

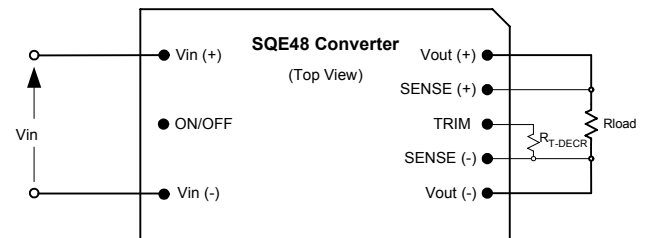
$$R_{T-DECR} = \frac{511}{|\Delta|} - 10.22 \text{ [k}\Omega\text{]}$$

where,

R<sub>T-DECR</sub> = Required value of trim-down resistor [kΩ] and Δ is defined above.

**Note:**

The above equations for calculation of trim resistor values match those typically used in conventional industry-standard quarter-bricks.



**Fig. D: Configuration for decreasing output voltage.**

Trimming/sensing beyond 110% of the rated output voltage is not an acceptable design practice, as this condition could cause unwanted triggering of the output overvoltage protection (OVP) circuit. The designer should ensure that the difference between the voltages across the converter's output pins and its sense pins does not exceed 10% of V<sub>OUT(NOM)</sub>, or:

$$[V_{OUT(+)} - V_{OUT(-)}] - [V_{SENSE(+)} - V_{SENSE(-)}] \leq V_{O-NOM} \times 10\% \text{ [V]}$$

This equation is applicable for any condition of output sensing and/or output trim.



## Protection Features

### Input Undervoltage Lockout

Input undervoltage lockout is standard with this converter. The converter will shut down when the input voltage drops below a pre-determined voltage.

The input voltage must be typically 34 V for the converter to turn on. Once the converter has been turned on, it will shut off when the input voltage drops typically below 32 V. This feature is beneficial in preventing deep discharging of batteries used in telecom applications.

### Output Overcurrent Protection (OCP)

The converter is protected against overcurrent or short circuit conditions. Upon sensing an overcurrent condition, the converter will switch to constant current operation and thereby begin to reduce output voltage.

If the converter is equipped with the special OCP version designated by the suffix K in the part number, the converter will shut down in approximately 15ms after entering the constant current mode of operation. The standard version (suffix 0) will continue operating in the constant current mode until the output voltage drops below 60% at which point the converter will shut down as shown in Figure 14.

Once the converter has shut down, it will attempt to restart nominally every 200 ms with a typical 3-5% duty cycle as shown in Figure 15. The attempted restart will continue indefinitely until the overload or short circuit conditions are removed or the output voltage rises above 40-50% of its nominal value.

Once the output current is brought back into its specified range, the converter automatically exits the hiccup mode and continues normal operation.

### Output Overvoltage Protection (OVP)

The converter will shut down if the output voltage across Vout(+) (Pin 8) and Vout(-) (Pin 4) exceeds the threshold of the OVP circuitry. The OVP circuitry contains its own reference, independent of the output voltage regulation loop. Once the converter has shut down, it will attempt to restart every 200 ms until the OVP condition is removed.

### Overtemperature Protection (OTP)

The converter will shut down under an overtemperature condition to protect itself from overheating caused by operation outside the thermal derating curves, or operation in abnormal conditions

such as system fan failure. Converter with the non-latching option will automatically restart after it has cooled to a safe operating temperature.

### Safety Requirements

The converters meet North American and International safety regulatory requirements per UL60950 and EN60950. Basic Insulation is provided between input and output.

The converters have no internal fuse. If required, the external fuse needs to be provided to protect the converter from catastrophic failure. Refer to the "Input Fuse Selection for DC/DC converters" application note on [www.power-one.com](http://www.power-one.com) for proper selection of the input fuse. Both input traces and the chassis ground trace (if applicable) must be capable of conducting a current of 1.5 times the value of the fuse without opening. The fuse must not be placed in the grounded input line.

Abnormal and component failure tests were conducted with the input protected by a 7A fuse. If a fuse rated greater than 7A is used, additional testing may be required. To protect a group of converters with a single fuse, the rating can be increased from the recommended value above.

### Electromagnetic Compatibility (EMC)

EMC requirements must be met at the end-product system level, as no specific standards dedicated to EMC characteristics of board mounted component dc-dc converters exist. However, Power-One tests its converters to several system level standards, primary of which is the more stringent EN55022, *Information technology equipment - Radio disturbance characteristics-Limits and methods of measurement*.

An effective internal LC differential filter significantly reduces input reflected ripple current, and improves EMC.

With the addition of a simple external filter, the SQE48T50012 converter passes the requirements of Class B conducted emissions per EN55022 and FCC requirements. Please contact Power-One Applications Engineering for details of this testing.

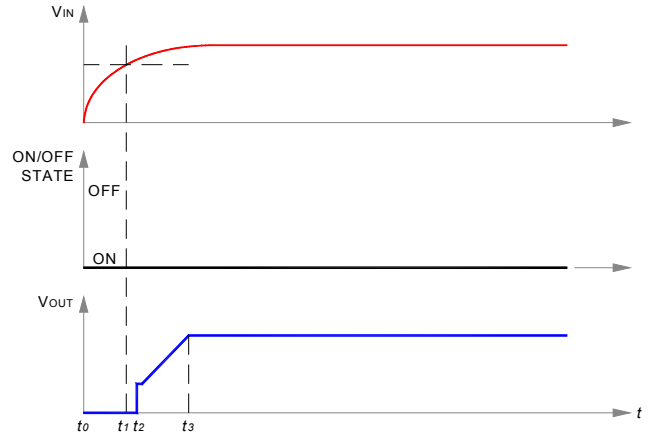
**Startup Information (using negative ON/OFF)**

**Scenario #1: Initial Startup From Bulk Supply**

ON/OFF function enabled, converter started via application of  $V_{IN}$ . See Figure E.

Time	Comments
$t_0$	ON/OFF pin is ON; system front-end power is toggled on, $V_{IN}$ to converter begins to rise.
$t_1$	$V_{IN}$ crosses undervoltage Lockout protection circuit threshold; converter enabled.
$t_2$	Converter begins to respond to turn-on command (converter turn-on delay).
$t_3$	Converter $V_{OUT}$ reaches 100% of nominal value.

For this example, the total converter startup time ( $t_3 - t_1$ ) is typically 3 ms.



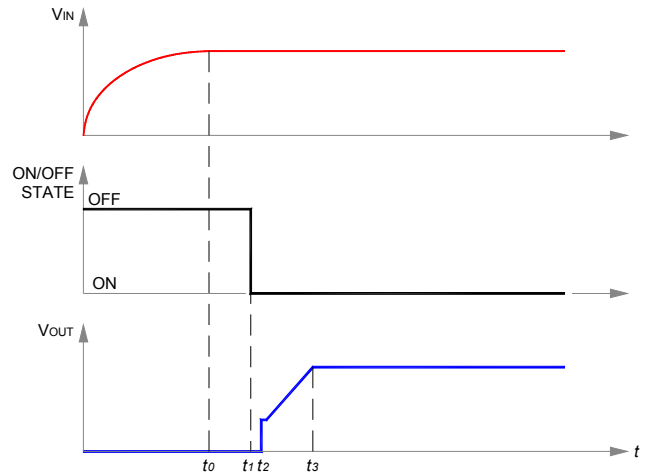
**Fig. E: Startup scenario #1.**

**Scenario #2: Initial Startup Using ON/OFF Pin**

With  $V_{IN}$  previously powered, converter started via ON/OFF pin. See Figure F.

Time	Comments
$t_0$	$V_{INPUT}$ at nominal value.
$t_1$	Arbitrary time when ON/OFF pin is enabled (converter enabled).
$t_2$	End of converter turn-on delay.
$t_3$	Converter $V_{OUT}$ reaches 100% of nominal value.

For this example, the total converter startup time ( $t_3 - t_1$ ) is typically 3 ms.



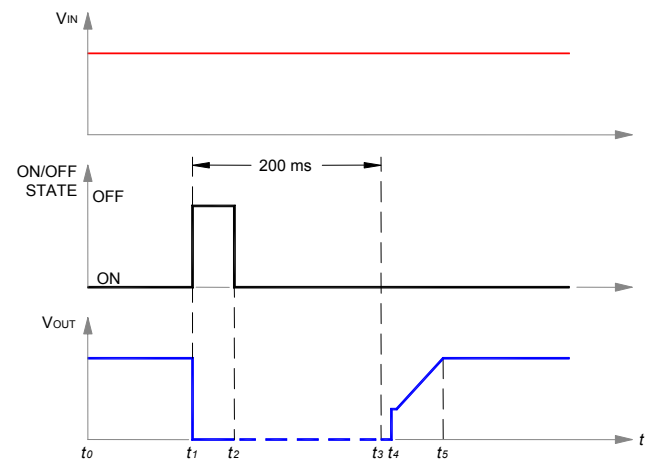
**Fig. F: Startup scenario #2.**

**Scenario #3: Turn-off and Restart Using ON/OFF Pin**

With  $V_{IN}$  previously powered, converter is disabled and then enabled via ON/OFF pin. See Figure G.

Time	Comments
$t_0$	$V_{IN}$ and $V_{OUT}$ are at nominal values; ON/OFF pin ON.
$t_1$	ON/OFF pin arbitrarily disabled; converter output falls to zero; turn-on inhibit delay period (200 ms typical) is initiated, and ON/OFF pin action is internally inhibited.
$t_2$	ON/OFF pin is externally re-enabled. If $(t_2 - t_1) \leq 200$ ms, external action of ON/OFF pin is locked out by startup inhibit timer. If $(t_2 - t_1) > 200$ ms, ON/OFF pin action is internally enabled.
$t_3$	Turn-on inhibit delay period ends. If ON/OFF pin is ON, converter begins turn-on; if off, converter awaits ON/OFF pin ON signal; see Figure F.
$t_4$	End of converter turn-on delay.
$t_5$	Converter $V_{OUT}$ reaches 100% of nominal value.

For the condition,  $(t_2 - t_1) \leq 200$  ms, the total converter startup time ( $t_5 - t_2$ ) is typically 203 ms. For  $(t_2 - t_1) > 200$  ms, startup will be typically 3 ms after release of ON/OFF pin.



**Fig. G: Startup scenario #3.**



## Characterization

### General Information

The converter has been characterized for many operational aspects, to include thermal derating (maximum load current as a function of ambient temperature and airflow) for vertical and horizontal mounting, efficiency, startup and shutdown parameters, output ripple and noise, transient response to load step-change, overload, and short circuit.

### Test Conditions

All data presented were taken with the converter soldered to a test board, specifically a 0.060" thick printed wiring board (PWB) with four layers. The top and bottom layers were not metalized. The two inner layers, comprised of two-ounce copper, were used to provide traces for connectivity to the converter.

The lack of metalization on the outer layers as well as the limited thermal connection ensured that heat transfer from the converter to the PWB was minimized. This provides a worst-case but consistent scenario for thermal derating purposes.

All measurements requiring airflow were made in the vertical and horizontal wind tunnel using Infrared (IR) thermography and thermocouples for thermometry.

Ensuring components on the converter do not exceed their ratings is important to maintaining high reliability. If one anticipates operating the converter at or close to the maximum loads specified in the derating curves, it is prudent to check actual operating temperatures in the application. Thermographic imaging is preferable; if this capability is not available, then thermocouples may be used. The use of AWG #40 gauge thermocouples is recommended to ensure measurement accuracy. Careful routing of the thermocouple leads will further minimize measurement error. Refer to Fig. H for the optimum measuring thermocouple locations.

### Thermal Derating

Load current vs. ambient temperature and airflow rates are given in Figure 1. Ambient temperature was varied between 25°C and 85°C, with airflow rates from 30 to 500 LFM (0.15 to 2.5 m/s).

For each set of conditions, the maximum load current was defined as the lowest of:

- (i) The output current at which any FET junction temperature does not exceed a maximum temperature of 120°C as indicated by the thermographic image, or

- (ii) The temperature of the transformer does not exceed 120°C, or
- (iii) The nominal rating of the converter (50A at 1.2 V).

During normal operation, derating curves with maximum FET temperature less or equal to 120°C should not be exceeded. Temperature at both thermocouple locations shown in Fig. H should not exceed 120°C in order to operate inside the derating curves.

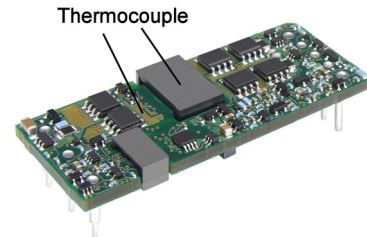


Fig. H: Locations of the thermocouple for thermal testing.

### Efficiency

Figure 2 shows the efficiency vs. load current plot for ambient temperature of 25 °C, airflow rate of 300 LFM (1.5 m/s) with vertical mounting and input voltages of 36 V, 48 V, and 72 V. Also, a plot of efficiency vs. load current, as a function of ambient temperature with  $V_{in} = 48 V$ , airflow rate of 200 LFM (1 m/s) with vertical mounting is shown in Figure 3.

### Power Dissipation

Figure 4 shows the power dissipation vs. load current plot for  $T_a = 25 ^\circ C$ , airflow rate of 300 LFM (1.5 m/s) with vertical mounting and input voltages of 36 V, 48 V, and 72 V. Also, a plot of power dissipation vs. load current, as a function of ambient temperature with  $V_{in} = 48V$ , airflow rate of 200 LFM (1 m/s) with vertical mounting is shown in Figure 5.

### Startup

Output voltage waveforms, during the turn-on transient using the ON/OFF pin for full rated load currents (resistive load) are shown without and with external load capacitance in Figure 6 and Figure 7

### Ripple and Noise

Figure 10 shows the output voltage ripple waveform, measured at full rated load current with a 10  $\mu F$  tantalum and 1 $\mu F$  ceramic capacitor across the output. Note that all output voltage waveforms are measured across a 1 $\mu F$  ceramic capacitor.

The input reflected-ripple current waveforms are obtained using the test setup shown in Figure 11. The corresponding waveforms are shown in Figure 12 and Figure 13.

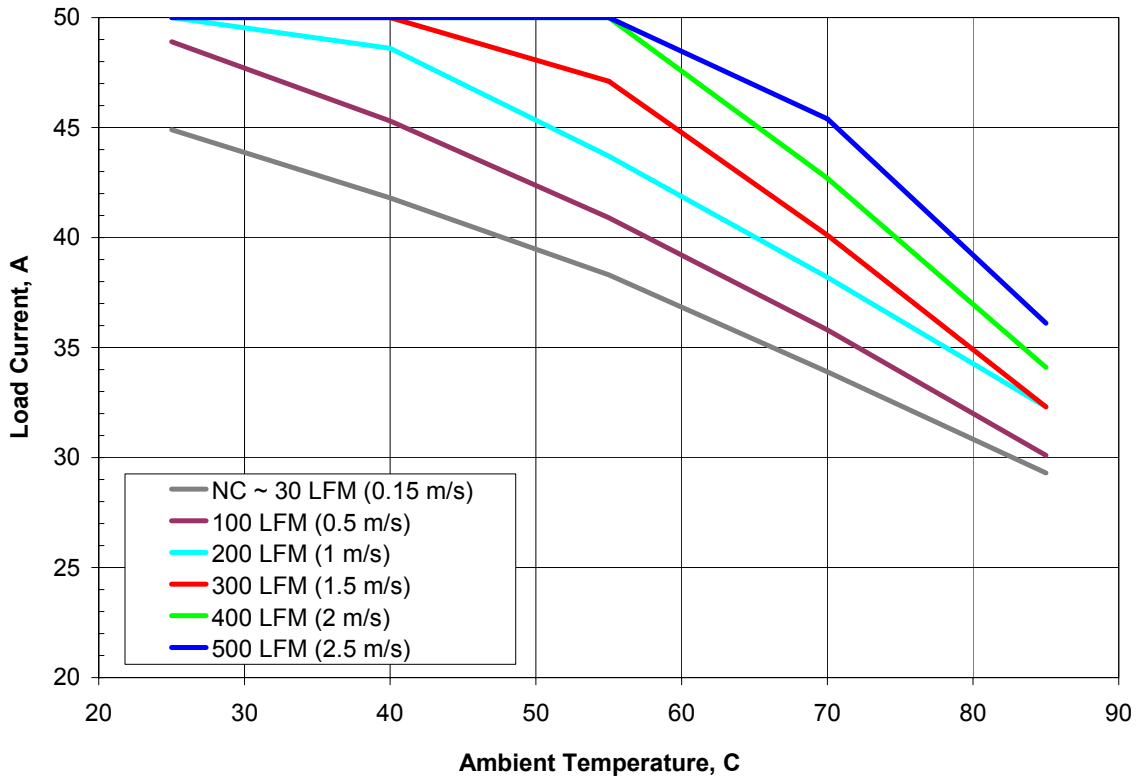


Figure 1. Available load current vs. ambient air temperature and airflow rates for SQE48T50012 converter mounted vertically with air flowing from pin 3 to pin 1, MOSFET temperature  $\leq 120$  °C,  $V_{in} = 48$  V.

Note: NC – Natural convection

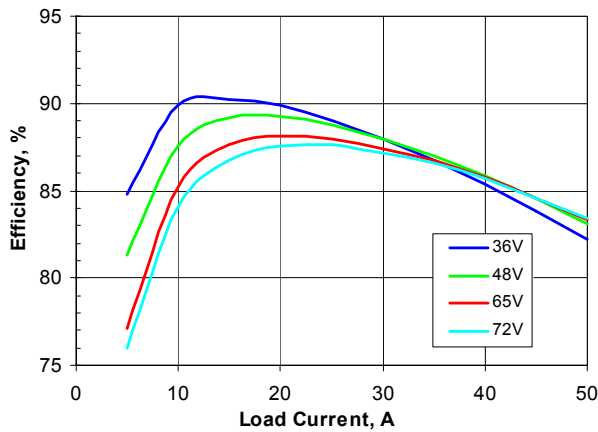


Figure 2. Efficiency vs. load current and input voltage for SQE48T50012 converter mounted vertically with air flowing from pin 3 to pin 1 at 300 LFM (1.5 m/s) and  $T_a=25$ °C.

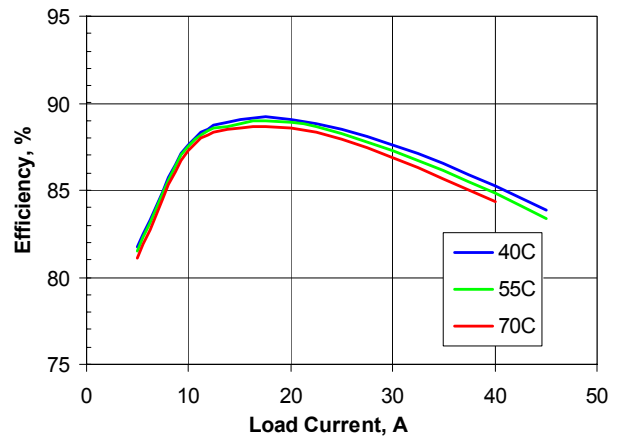
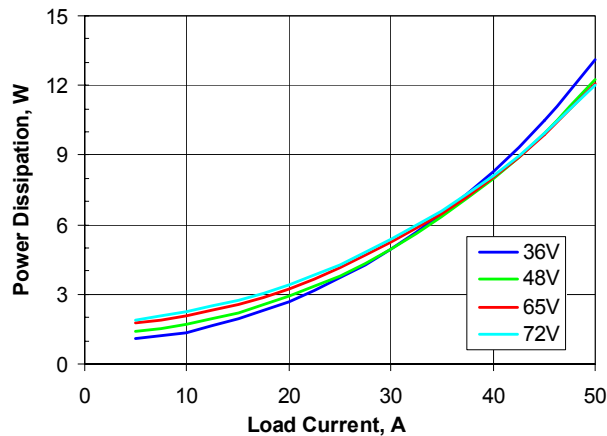
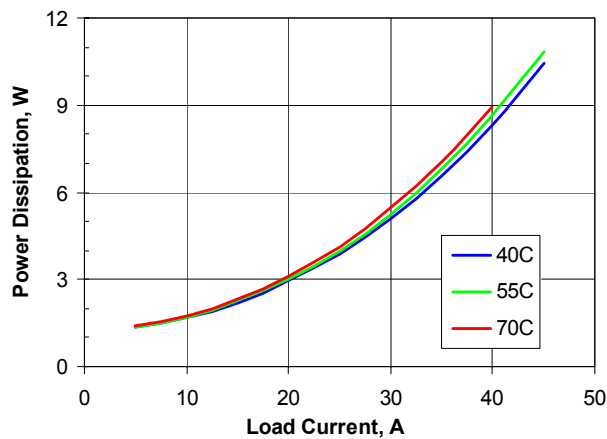


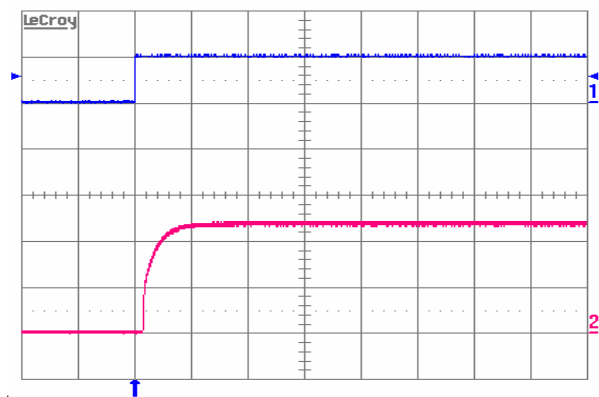
Figure 3. Efficiency vs. load current and ambient temperature for SQE48T50012 converter mounted vertically with  $V_{in}=48$ V and air flowing from pin 3 to pin 1 at 200LFM (1.0m/s).



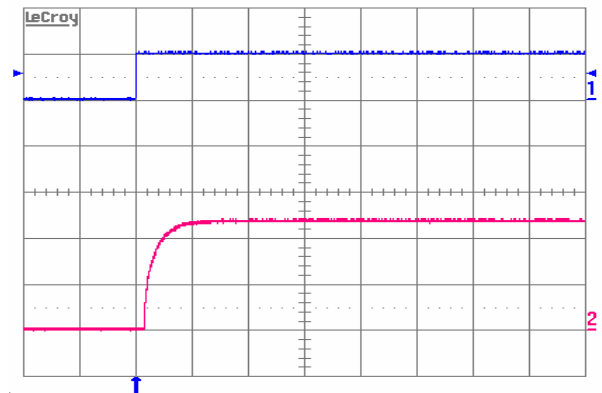
**Figure 4.** Power dissipation vs. load current and input voltage for SQE48T50012 converter mounted vertically with air flowing from pin 3 to pin 1 at a rate of 300 LFM (1.5 m/s) and  $T_a = 25^\circ\text{C}$ .



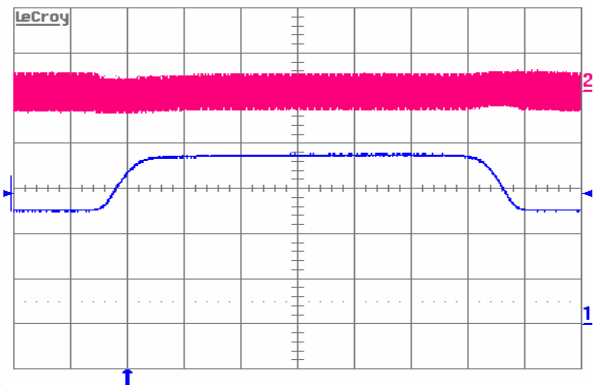
**Figure 5.** Power dissipation vs. load current and ambient temperature for SQE48T50012 converter mounted vertically with  $V_{in} = 48\text{ V}$  and air flowing from pin 3 to pin 1 at a rate of 200 LFM (1.0 m/s).



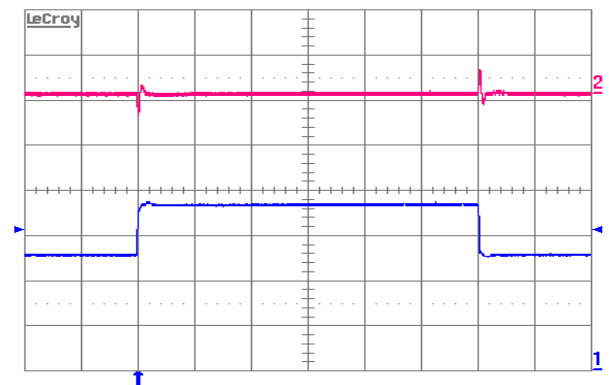
**Figure 6.** Turn-on transient at full rated load current (resistive) with no output capacitor at  $V_{in} = 48\text{ V}$ , triggered via ON/OFF pin. Top trace: ON/OFF signal (5 V/div.). Bottom trace: Output voltage (0.5 V/div.). Time scale: 5 ms/div.



**Figure 7.** Turn-on transient at full rated load current (resistive) plus 10,000  $\mu\text{F}$  at  $V_{in} = 48\text{ V}$ , triggered via ON/OFF pin. Top trace: ON/OFF signal (5 V/div.). Bottom trace: Output voltage (0.5 V/div.). Time scale: 5 ms/div.



**Figure 8.** Output voltage response to load current step-change (25 A – 37.5 A – 25 A) at  $V_{in} = 48\text{ V}$ . Top trace: output voltage (20 mV/div.). Bottom trace: load current (10 A/div.). Current slew rate: 0.1 A/ $\mu\text{s}$ .  $C_o = 1\text{ }\mu\text{F}$  ceramic. Time scale: 0.2ms/div.



**Figure 9.** Output voltage response to load current step-change (25 A – 37.5 A – 25 A) at  $V_{in} = 48\text{ V}$ . Top trace: output voltage (100 mV/div.). Bottom trace: load current (10 A/div.). Current slew rate: 2.5 A/ $\mu\text{s}$ .  $C_o = 470\text{ }\mu\text{F POS} + 1\text{ }\mu\text{F}$  ceramic. Time scale: 0.2 ms/div.

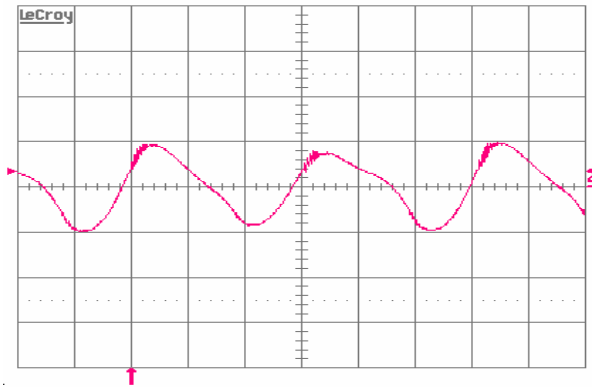


Figure 10. Output voltage ripple (20 mV/div.) at full rated load current into a resistive load with  $C_o = 10 \mu\text{F}$  tantalum +  $1 \mu\text{F}$  ceramic and  $V_{in} = 48 \text{ V}$ . Time scale:  $1 \mu\text{s}/\text{div}$ .

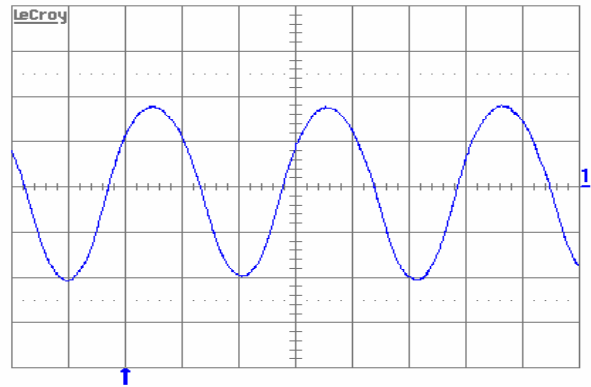


Figure 13. Input reflected ripple-current,  $i_c$  (100 mA/div.), measured at input terminals at full rated load current and  $V_{in} = 48 \text{ V}$ . Refer to Figure 11 for test setup. Time scale:  $1 \mu\text{s}/\text{div}$ .

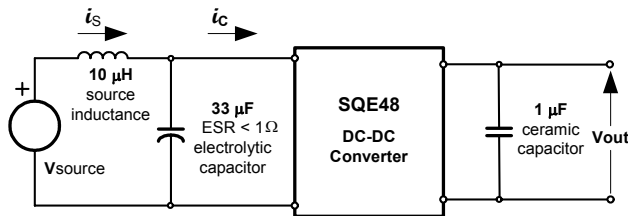


Figure 11. Test setup for measuring input reflected ripple currents,  $i_c$  and  $i_s$ .

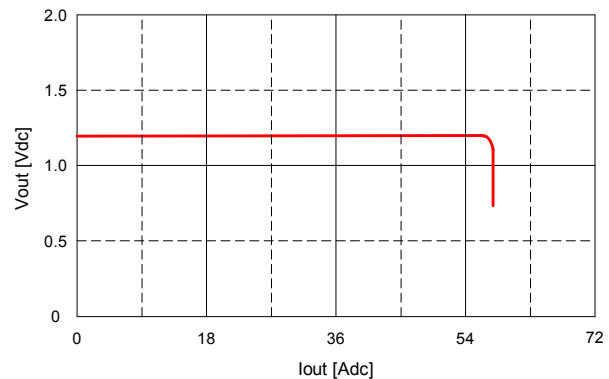


Figure 14. Output voltage vs. load current showing current limit point and converter shutdown point. Input voltage has almost no effect on current limit characteristic.

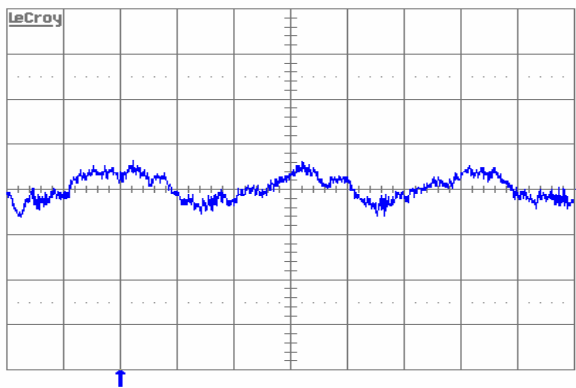


Figure 12. Input reflected-ripple current,  $i_s$  (10 mA/div.), measured through  $10 \mu\text{H}$  at the source at full rated load current and  $V_{in} = 48 \text{ V}$ . Refer to Figure 11 for test setup. Time scale:  $1 \mu\text{s}/\text{div}$ .

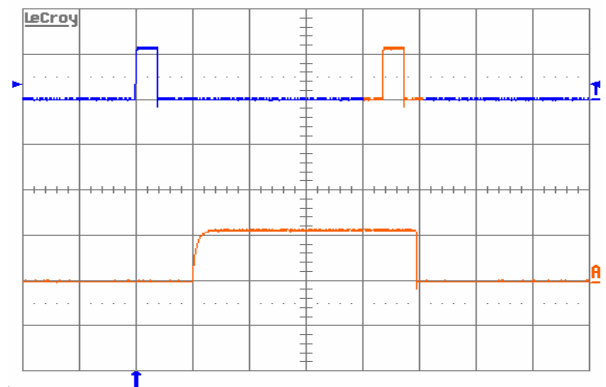
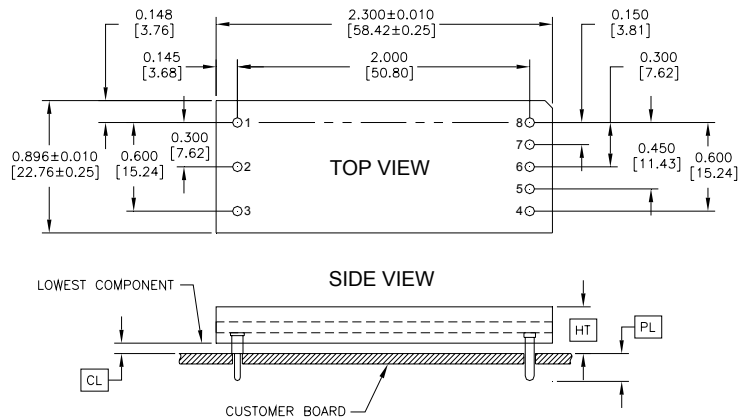


Figure 15. Load current (top trace, 50 A/div., 50 ms/div.) into a  $10 \text{ m}\Omega$  short circuit during restart, at  $V_{in} = 48 \text{ V}$ . Bottom trace (50 A/div., 5 ms/div.) is an expansion of the on-time portion of the top trace.

**Physical Information**

**SQE48T Pinout (Through-hole)**



Pad/Pin Connections	
Pad/Pin #	Function
1	Vin (+)
2	ON/OFF
3	Vin (-)
4	Vout (-)
5	SENSE(-)
6	TRIM
7	SENSE(+)
8	Vout (+)

Height Option	HT (Max. Height)	CL (Min. Clearance)
	+0.000 [+0.00] -0.038 [-0.97]	+0.016 [+0.41] -0.000 [-0.00]
D	0.374 [9.5]	0.045 [1.14]

Pin Option	PL Pin Length
	±0.005 [±0.13]
A	0.188 [4.78]
B	0.145 [3.68]

**SQE48T Platform Notes**

- All dimensions are in inches [mm]
- Pins 1-3 and 5-7 are Ø 0.040" [1.02] with Ø 0.078" [1.98] shoulder
- Pins 4 and 8 are Ø 0.062" [1.57] without shoulder
- Pin Material: Brass Alloy 360
- Pin Finish: Tin over Nickel

**Converter Part Numbering/Ordering Information**

Product Series	Input Voltage	Mounting Scheme	Rated Current	Output Voltage	ON/OFF Logic	Maximum Height [HT]	Pin Length [PL]	Special Features	RoHS
<b>SQE</b>	<b>48</b>	<b>T</b>	<b>50</b>	<b>012</b>	<b>-</b>	<b>D</b>	<b>A</b>	<b>K</b>	<b>G</b>
One-Eighth Brick Format	36-75 V	T ⇒ Through-hole	50 ⇒ 50 ADC	012 ⇒ 1.2 V	N ⇒ Negative P ⇒ Positive	D ⇒ 0.374"	Through hole A ⇒ 0.188" B ⇒ 0.145"	0 ⇒ 2250VDC isolation, no CM cap K ⇒ 1500VDC isolation, CM cap, and special OCP	No Suffix ⇒ RoHS lead-solder-exemption compliant G ⇒ RoHS compliant for all six substances

The example above describes P/N SQE48T50012-NDAKG: 36-75 V input, through-hole, 50A @ 1.2V output, negative ON/OFF logic, maximum height of 0.374", 0.188" pins, 1500VDC isolation, common mode capacitor, special OCP, and RoHS compliant for all 6 substances. Consult factory for availability of other options.

**Notes:**

1. NUCLEAR AND MEDICAL APPLICATIONS - Power-One products are not designed, intended for use in, or authorized for use as critical components in life support systems, equipment used in hazardous environments, or nuclear control systems without the express written consent of the respective divisional president of Power-One, Inc.
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